

Memo

To: City of Toronto, Development Engineering

From: Dorothy Poon, P.Eng. Counterpoint Engineering

Wessal Omarkhail, Choice Grosvenor/Grenville Inc. cc:

Date: June 6, 2025

Subject: 26 Grenville Street & 27 Grosvenor Street, Servicing Memo Addendum

Our File: 24-18045

This Memo has been prepared to discuss the servicing impact of the updated unit count/mix as shown on the architectural plans dated June 6, 2025.

Based on the June 6, 2025 architectural plans, the proposed development at 26 Grenville Street and 27 Grosvenor Street will have a total of 769 units compared to 770 units as indicated in all servicing demand calculations in the 'Functional Servicing and Stormwater Management Implementation Report' dated December 6, 2021 prepared by our office.

Based on the decrease in the total units, the water demand and sanitary demand calculations have been reviewed and updated to determine if the municipal infrastructure can accommodate the site and what external upgrades, if any, would be required. It should be noted that the increase in units does not have a fundamental impact on the proposed stormwater management design and therefore that component of the previously submitted Report was not reviewed.

Tower A water demand increases from 4,069 L/min to 4,106 L/min and Tower B Water demand increases from 4,114 L/min to 4,135 L/min, both of which is a marginal increase. Based on the previously completed flow test results, there is sufficient flow in the existing municipal watermain system to accommodate the updated total water demand.

The new equivalent population based on the unit count decrease is 1407 persons compared to 1511 persons as used in calculations in the December 6, 2021 Report. Based on this decrease in population, the new peak sanitary flow has been calculated to be 15.06 L/s compared to 16.25 L/s in the December 6, 2021 Report. Since the proposed unit count increase results in a decrease in peak sanitary flow, the proposed catchbasin disconnection at St. Nicholas Street can still provide the required 2:1 offset.

Given the above, it is our opinion that the increase in unit counts does not have any fundamental change on the conclusions discussed in our December 6, 2021 Report. No external upgrades, other than those already proposed in our December 6, 2021 Report, would be required to the municipal watermain, municipal storm sewer, and municipal sanitary sewer systems.

Sincerely,

Dorothy Poon, P.Eng.

Associate | Team Lead, Engineering Toronto

416-806-3325

dpoon@counterpointeng.com

APPENDIX A

SUPPORTING CALCULATIONS

Water Demand Design Calculations

Project: 27 Grosvenor & 26 Grenville - Tower A Demands

Project No: 18045

Location: Toronto, Ontario
Site Area: 0.3846 ha

Population

1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

	Residential Units			
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units
TOTAL UNITS / AREA (m ²)	279	62	31	372

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	391	131	97	619
Total Equivalent Population				619

City of Toronto Watermain Guidelines

Per Capita Demand

Single Family	310	(L/capita/day)
Multi-Unit	190	(L/capita/day)

Peaking Factors

Land Use	Minimum Hour	Maximum Hour	Maximum Day
Residential	0.80	2.25	1.50
Commercial	0.84	1.20	1.10
Industrial	0.84	1.90	1.10
Institutional	0.84	1.90	1.10
Apartment	0.84	2.50	1.30

*Values used for Residential (Multi-Unit) Land Use

Water Demand based on Equivalent Population

Land Use	Population	Minimum Hour (L/min)	Maximum Hour (L/min)	Maximum Day (L/min)	Fire Flow Required (L/min)	Fire Flow Duration (hr)*	Max Day + Fire Flow (L/min)
Residential (Multi-Unit)	619	68.6	204.2	106.2	-	-	-
Totals	619	68.6	204.2	106.2	4000	2.00	4,106.2

REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Fire Underwriters Survey

27 Grosvenor & 26 Grenville - Tower A Demands Project:

Project No: 18045

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$
 where F=

the required fire flow in litres per minute.
coefficient related to the type of construction.
= 1.5 for wood frame construction (structure essentially all combustible).

= 1.0 for ordinary construction (brick or other masonry walls, combustible floor and

= 0.8 for non-combustible construction (unprotected metal structural masonry or metal walls).

= 0.6 for fire-resistive construction (fully protected frame, floors, roof).

The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

1	Type of Construction	Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

	Contents	% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
С	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

Fire Flow 1)

Type of Construction:

C=

A*= F=

FC	
0.6	
1628	m ²
5,326	L/min

5,000 L/min (round to the nearest 1,000L/min)

*Note: Building will be fire restive as per OBC requirements with protected vertical openings. Area is the total of the largest floor (Level 1) plus 25% of the next 2 adjoining floors above.

2) Occupancy Reduction/Surcharge

Contents Factor: Reduction/Surcharge of

-25% 5000L/min + -1331

3669L/min -

-1,331 L/min = L/min = 3,669 L/min

3) System Type Reduction

NFPA 13 Sprinkler: Standard Water Supply:

Fully Supervised: Total

Reduction of

50% 50% L/min = 1,834 L/min =

30%

10%

10%

YES

YES

YES

1,834 L/min 1,834 L/min

4) **Separation Charge**

Total

Building Face North East South West

Dist(m)	Charge
26.1	10%
0.0	25%
8.4	20%
12.0	15%

70% of 3668.6 L/min = 2,568 L/min (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

1834L/min +

2568L/min

4,402 L/min (2,000L/min<F<45,000L/min)

F=	4,000	L/min	(r
F=	67	L/s	
F=	1,057	gpm	

round to the nearest 1,000L/min)

counterpoint engineering

NFPA Theoretical Flow Calculations

Project Name: 27 Grosvenor & 26 Grenville - Tower A Demands

Project Number: 18045

Based on National Fire Protection Association Guidelines, the available flow at the minimum residual pressure of 20psi can be calculated based on the observed flow at the observed pressure readings, as follows:

$$Q_F = 29.83 \text{ x c x d}^2 \text{ x p}^{0.5}$$
 , where

 Q_F = observed flow (US GPM)

c = hydrant nozzle coefficient (0.90 - 0.95)

d = nozzle diameter (in)

p = observed pitot pressure

$$Q_R = Q_F x h_F^{0.54} / h_R^{0.54}$$
 , where

Q_R = available flow

 Q_F = observed flow (US GPM)

h_F = drop from measured static to desired baseline pressure

h_R = drop from measured static to measured residual pressure

Based on flow test results obtained by Lozzi Aqua Check dated September 4, 2019 on the Grosvenor watermair

$$c = 0.95$$

$$d = 2.5 \text{ in}$$

$$number of ports = 2$$

$$p = 5$$

$$Q_F = 792 \text{ US GPM}$$

Measured Static Pressure = 55 psi
Measured Residual Pressure = 37 psi

Desired Residual Pressure = 20 psi , minimum per City of Toronto design criteria

Q_R = 1134 US GPM per fire conneciton 4,294 L/min

Water Demand Design Calculations

Project: 27 Grosvenor & 26 Grenville - Tower B

Project No: 18045

Location: Toronto, Ontario
Site Area: 0.3846 ha

Population

1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²
Schools	0.0258	persons/m ²

	Residential Units			Childcare	
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)
TOTAL UNITS / AREA (m ²)	216	92	89	397	669

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	303	194	276	773
Institutional	-	-	-	18
Total Equivalent Populatio	791			

City of Toronto Watermain Guidelines

Per Capita Demand

Single Family	310	(L/capita/day)
Multi-Unit	190	(L/capita/day)

Peaking Factors

Land Use	Minimum Hour	Maximum Hour	Maximum Day
Residential	0.80	2.25	1.50
Commercial	0.84	1.20	1.10
Industrial	0.84	1.90	1.10
Institutional	0.84	1.90	1.10
Apartment	0.84	2.50	1.30

*Values used for Institutional Land Use *Values used for Residential (Multi-Unit) Land Use

Water Demand based on Equivalent Population

Land Use	Population	Minimum Hour (L/min)	Maximum Hour (L/min)	Maximum Day (L/min)	Fire Flow Required (L/min)	Fire Flow Duration (hr)*	Max Day + Fire Flow (L/min)
Institutional	18	2.0	4.5	2.6	-	-	-
Residential (Multi-Unit)	773	85.7	255.0	132.6	-	-	-
Totals	791	87.7	259.5	135.2	4000	2.00	4,135.2

REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Fire Underwriters Survey

27 Grosvenor & 26 Grenville - Tower B Project:

Project No: 18045

Guide for Determination of Required Flow Copyright I.S.O

$$F = 220C\sqrt{A}$$
 where F = C =

the required fire flow in litres per minute.
coefficient related to the type of construction.
= 1.5 for wood frame construction (structure essentially all combustible).

= 1.0 for ordinary construction (brick or other masonry walls, combustible floor and

= 0.8 for non-combustible construction (unprotected metal structural

masonry or metal walls).
= 0.6 for fire-resistive construction (fully protected frame, floors, roof).

The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Т	ype of Construction	Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

	Contents	% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
С	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) Fire Flow

Type of Construction:

C= A*=

F=

0.6 m² 1589 5,261 L/min

5,000 L/min (round to the nearest 1,000L/min)

*Note: Building will be fire restive as per OBC requirements with protected vertical openings. Area is the total of the largest floor (Level 1) plus 25% of the next 2 adjoining floors above.

2) Occupancy Reduction/Surcharge

Contents Factor: Reduction/Surcharge of

-25% 5000L/min + -1315 L/min =

YES

YES

YES

-1,315 L/min = 3,685 L/min

30%

10%

10%

50%

3) System Type Reduction

NFPA 13 Sprinkler: Standard Water Supply:

Fully Supervised:

Total Reduction of

50% L/min = 1,842 L/min = 3685L/min -

1,842 L/min 1,842 L/min

4) **Separation Charge**

Total

Building Face North East South West

Dist(m)	Charge
8.4	20%
11.5	15%
24.1	10%
5.5	20%

65% of 3684.8 L/min = 2,395 L/min (max exposure charge can be 75%)

Separation	Charge	Separation	Charge
0 to 3m	25%	20.1 to 30 m	10%
3.1 to 10m	20%	30.1 to 45m	5%
10.1 to 20m	15%		

1842L/min +

2395L/min

4,237 L/min (2,000L/min<F<45,000L/min)

F=	4,000	L/min
F=	67	L/s
F=	1,057	gpm

(round to the nearest 1,000L/min)

counterpoint engineering

NFPA Theoretical Flow Calculations

Project Name: 27 Grosvenor & 26 Grenville - Tower B

Project Number: 18045

Based on National Fire Protection Association Guidelines, the available flow at the minimum residual pressure of 20psi can be calculated based on the observed flow at the observed pressure readings, as follows:

$$Q_F = 29.83 \times c \times d^2 \times p^{0.5}$$
, where

 Q_F = observed flow (US GPM)

c = hydrant nozzle coefficient (0.90 - 0.95)

d = nozzle diameter (in)

p = observed pitot pressure

$$Q_R = Q_F x h_F^{0.54} / h_R^{0.54}$$
 , where

 Q_R = available flow

 Q_F = observed flow (US GPM)

h_F = drop from measured static to desired baseline pressure

h_R = drop from measured static to measured residual pressure

Based on flow test results obtained by Lozzi Aqua Check dated September 4, 2019 for the Grenville watermain

$$c = 0.95$$

$$d = 2.5 \text{ in}$$

$$number of ports = 2$$

$$p = 25$$

$$Q_F = 1771 US GPM$$

Measured Static Pressure = 56 psi

Measured Residual Pressure = 40 psi

Desired Residual Pressure = 20 psi

Desired Residual Pressure = 20 psi , minimum per City of Toronto design criteria

Q_R = 2744 US GPM per fire conneciton 10,388 L/min

Project: 27 Grosvenor & 26 Grenville

Project No: 18045

Location: Toronto Ontario **Site Area:** 0.3846

Existing Equivalent Population Calculations

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

Single Family Dwelling	3.5	ppu
Duplex	2.3	ppu
1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

	Residential Units		Office
	Single Family Dwelling	Duplex Units	Area (m²)
Existing 2 Storey Office (26 Grenville)	0	-	2362
TOTAL UNITS / AREA (m ²)	3	0	2362

	Single Family Dwelling	TOTAL POPULATION
Residential	0	0
Office	=	77.946
Total Equivalent Population		78

Peak flow Design Parameters

Industrial/Commercial/Office	240	litres/person/day
Infiltration	0.26	litres/second/ha

Harmon Peaking Factor

	Harmon
Total Population	Peak Factor
78	4.27

Average Dry Weather Flow	0.22	L/s
Total Peak Wastewater Flow	0.92	L/s
Infiltration	0.10	L/s
_		
Flow	1.02	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (Entire Development)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²
Schools	0.0258 persons/m ²

	Residential Units				Childcare
	1B / 1B+D 2B / 2B + D 3B / 3B+D Total Units		Area (m²)		
TOTAL UNITS / AREA (m ²)	495 154 120 769				669

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	693	324	372	1389
Institutional	-	-	-	18
Total Equivalent Population				1407

Peak flow Design Parameters

Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

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	Harmon Peak
Residential Population	Factor
1389	3.70

Residential Flow	14.29	L/s	*based on population
Institutional Flow	0.14	L/s	*based on floor area
Groundwater Flows	0.63	L/s	* 10 USGPM pump

Flow	15.06	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (Tower A)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²

	Residential Units			
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units
TOTAL UNITS / AREA (m ²)	279	62	31	372

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	391	131	97	619
Total Equivalent Population				619

Peak flow Design Parameters

Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

	Harmon Peak
Residential Population	Factor
619	3.92

Residential Flow	6.75	L/s	*based on population
Retail Flow	0.00	L/s	*based on floor area
Groundwater Flows	0.63	L/s	* 10 USGPM pump

Flow	7.38	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (Tower B)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²
Schools	0.0258 persons/m ²

	Residential Units				Childcare
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)
TOTAL UNITS / AREA (m ²)	216	92	89	397	669

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	303	194	276	773
Childcare	-	-	-	18
Total Equivalent Population				791

Peak flow Design Parameters

Residential Average flow	240 litres/person/day
Institutional Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

, , , , , , , , , , , , , , , , , , , ,	
	Harmon Peak
Residential Population	Factor
773	3.87

Residential Flow	8.31	L/s	*based on population
Institutional Flow	0.14	L/s	*based on floor area
Groundwater Flows	0.00	L/s	

Flow	8.45	L/s

APPENDIX B

SUPPORTING CALCULATIONS FROM 'FUNCTIONAL SERVICIGN AND STORMWATER MANAGEMENT IMPLEMENTATION REPORT' DATED DECEMBER 6, 2021

Water Demand Design Calculations

Project: 27 Grosvenor & 26 Grenville - North Tower Demands

Project No: 18045

Location: Toronto, Ontario
Site Area: 0.3846 ha

Population

· opulation		
1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

	Residential Units				Commercial
	1B / 1B+D				Area (m²)
TOTAL UNITS / AREA (m ²)	80	101	25	206	0.0

		Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential		112	213	78	403
Commercial		-	-	-	0
Total Equivalent Population					403

City of Toronto Watermain Guidelines

Per Capita Demand

Single Family	310	(L/capita/day)
Multi-Unit	190	(L/capita/day)

Peaking Factors

Land Use	Minimum Hour	Maximum Hour	Maximum Day	
Residential	0.80	2.25	1.50	
Commercial	0.84	1.20	1.10	*Values ι
Industrial	0.84	1.90	1.10	
Institutional	0.84	1.90	1.10	
Apartment	0.84	2.50	1.30	*Values ι

*Values used for Commercial Land Use

*Values used for Residential (Multi-Unit) Land Use

Water Demand based on Equivalent Population

Land Use	Population	Minimum Hour (L/min)	Maximum Hour (L/min)	Maximum Day (L/min)	Fire Flow Required (L/min)	Fire Flow Duration (hr)*	Max Day + Fire Flow (L/min)
Commercial	0	0.0	0.0	0.0	-	1	-
Residential (Multi-Unit)	403	44.7	132.9	69.1	-	-	-
Totals	403	44.7	132.9	69.1	4000	2.00	4,069.1

REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Fire Underwriters Survey

Project: 27 Grosvenor & 26 Grenville - North Tower Demands

Project No:

Guide for Determination of Required Flow Copyright I.S.O

 $F = 220C\sqrt{A}$ where

the required fire flow in litres per minute.

coefficient related to the type of construction.

1.5 for wood frame construction (structure essentially all combustible).

1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior). = 0.8 for non-combustible construction (unprotected metal structural components,

masonry or metal walls).

= 0.6 for fire-resistive construction (fully protected frame, floors, roof).

The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Т	ype of Construction	Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

	Contents	% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
С	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) Fire Flow

Type of Construction:

C= A*= F=

0.6 1175 4,524 L/min

5,000 L/min (round to the nearest 1,000L/min)

*Note: Building will be fire restive as per OBC requirements with protected vertical openings. Area is the total of the largest floor (Level 12) plus 25% of the next 2 adjoining floors above.

2) Occupancy Reduction/Surcharge

Contents Factor: Reduction/Surcharge of

NC -25% 5000L/min + -1131

-1,131 L/min 3,869 L/min L/min =

30%

10%

10%

50%

System Type Reduction 3)

Reduction of

NFPA 13 Sprinkler: Standard Water Supply:

Fully Supervised: Total

50% L/min 3869L/min -1,935 L/min =

YES

YES

1,935 L/min 1.935 L/min

Separation Charge 4)

Total

Building Face North East South West

Dist(m)	Charge
26.1	10%
5.3	20%
21.0	10%
19.1	15%
	FF0/

55% of 3869.1 L/min = 2,128 L/min (max exposure charge can be 75%)

Separation Separation Charge Charge 0 to 3m 3.1 to 10m 20.1 to 30 m 30.1 to 45m 10% 20% 5% 10.1 to 20m

1935L/min + 2128L/min 4,063 L/min (2,000L/min<F<45,000L/min)

F=	4,000	L/min	(rou
F=	67	L/s	
F=	1,057	gpm	

nd to the nearest 1,000L/min)

counterpoint engineering

NFPA Theoretical Flow Calculations

Project Name: 27 Grosvenor & 26 Grenville - North Tower Demands

Project Number: 18045

Based on National Fire Protection Association Guidelines, the available flow at the minimum residual pressure of 20psi can be calculated based on the observed flow at the observed pressure readings, as follows:

$$Q_F = 29.83 \text{ x c x d}^2 \text{ x p}^{0.5}$$
, where

 Q_F = observed flow (US GPM)

c = hydrant nozzle coefficient (0.90 - 0.95)

d = nozzle diameter (in)

p = observed pitot pressure

$$Q_R = Q_F x h_F^{0.54} / h_R^{0.54}$$
 , where

 Q_R = available flow

 Q_F = observed flow (US GPM)

h_F = drop from measured static to desired baseline pressure

h_R = drop from measured static to measured residual pressure

Based on flow test results obtained by Lozzi Aqua Check dated September 4, 2019 on the Grosvenor watermain

$$c = 0.9$$

$$d = 2.5 \text{ in}$$

$$number of ports = 2$$

$$p = 5$$

$$Q_F = 750 \text{ US GPM}$$

Measured Static Pressure = 55 psi
Measured Residual Pressure = 37 psi
Desired Residual Pressure = 20 psi

Pressure = 20 psi , minimum per City of Toronto design criteria

Q_R = 1075 US GPM per fire conneciton 4,068 L/min

Water Demand Design Calculations

Project: 27 Grosvenor & 26 Grenville - South Tower

Project No: 18045

Location: Toronto, Ontario Site Area: 0.3846 ha

Population

· opaiation		
1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

		Commercial			
	1B / 1B+D				Area (m²)
TOTAL UNITS / AREA (m ²)	198	165	12	375	0.0

		Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential		278	347	38	663
Commercial		-	-	-	0
Total Equivalent Population					

City of Toronto Watermain Guidelines

Per Capita Demand

Single Family	310	(L/capita/day)
Multi-Unit	190	(L/capita/day)

Peaking Factors

Land Use	Minimum Hour	Maximum Hour	Maximum Day	
Residential	0.80	2.25	1.50	
Commercial	0.84	1.20	1.10	*Values used for Commercial Land Use
Industrial	0.84	1.90	1.10	
Institutional	0.84	1.90	1.10	
Apartment	0.84	2.50	1.30	*Values used for Residential (Multi-Unit)

Residential (Multi-Unit) Land Use

Water Demand based on Equivalent Population

Land Use	Population	Minimum Hour (L/min)	Maximum Hour (L/min)	Maximum Day (L/min)	Fire Flow Required (L/min)	Fire Flow Duration (hr)*	Max Day + Fire Flow (L/min)
Commercial	0	0.0	0.0	0.0	-	1	-
Residential (Multi-Unit)	663	73.5	218.7	113.7	-	-	-
Totals	663	73.5	218.7	113.7	4000	2.00	4,113.7

REQUIRED FIRE FLOW WORKSHEET - PROPOSED DEVELOPMENT

Fire Underwriters Survey

Project: 27 Grosvenor & 26 Grenville - South Tower

Project No: 18045

Guide for Determination of Required Flow Copyright I.S.O

 $F = 220C\sqrt{A}$ where

the required fire flow in litres per minute.

coefficient related to the type of construction.

1.5 for wood frame construction (structure essentially all combustible).

1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior).

= 0.8 for non-combustible construction (unprotected metal structural components, masonry or metal walls).

= 0.6 for fire-resistive construction (fully protected frame, floors, roof).

The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building being considered.

Т	ype of Construction	Class Factor
WF	Wood Frame	1.5
OC	Ordinary Construction	1.0
NC	Non-Combustible	0.8
FC	Fire-Resistive	0.6

Area Notes for Fire Resistive Buildings (from FUS manual, 1999):

If Vertical Openings are inadequately protected (less than 1-hour fire rating): Area is the total of the two largest adjoining floors (above ground level) plus 50% of the area of each of the next 8 adjoining floors above that.

	Contents	% Reduction
NC	Non-Combustible	25
LC	Limited Combustible	15
С	Combustible	0
FB	Free Burning	15
RB	Rapid Burning	25

If Vertical Openings are adequately protected (at least 1-hour fire rating): Area is the total of the largest floor (above ground level) plus 25% of the area of each of the next 2 immediately adjoining floors above that.

1) Fire Flow

Type of Construction:

C= A*= F=

0.6 1175 4,524 L/min

5,000 L/min (round to the nearest 1,000L/min)

*Note: Building will be fire restive as per OBC requirements with protected vertical openings. Area is the total of the largest floor (Level 12) plus 25% of the next 2 adjoining floors above.

2) Occupancy Reduction/Surcharge

Contents Factor: Reduction/Surcharge of

NC -25% 5000L/min +

YES

YES

-1,131 L/min 3,869 L/min -1131 L/min =

System Type Reduction 3)

> NFPA 13 Sprinkler: Standard Water Supply:

Fully Supervised: Total

50% L/min 3869L/min -1,935

30% 10% 10% 50%

Reduction of

L/min =

1,935 L/min 1.935 L/min

Separation Charge 4)

Building Face North East South West Total

Dist(m)	Charge
14.2	15%
12.6	15%
24.1	10%
5.6	20%
	500/

60% of 3869.1 L/min = 2,321 L/min (max exposure charge can be 75%)

Separation	Charge	Separation	Charge	
0 to 3m	25%	20.1 to 30 m	10%	
3.1 to 10m	20%	30.1 to 45m	5%	
10.1 to 20m	15%			

1935L/min +

2321L/min

4,256 L/min (2,000L/min<F<45,000L/min)

F=	4,000	L/min
F=	67	L/s
F=	1,057	gpm

(round to the nearest 1,000L/min)

counterpoint engineering

NFPA Theoretical Flow Calculations

Project Name: 27 Grosvenor & 26 Grenville - South Tower

Project Number: 18045

Based on National Fire Protection Association Guidelines, the available flow at the minimum residual pressure of 20psi can be calculated based on the observed flow at the observed pressure readings, as follows:

$$Q_F = 29.83 \text{ x c x d}^2 \text{ x p}^{0.5}$$
 , where

 Q_F = observed flow (US GPM)

c = hydrant nozzle coefficient (0.90 - 0.95)

d = nozzle diameter (in)

p = observed pitot pressure

$$Q_R = Q_F x h_F^{0.54} / h_R^{0.54}$$
 , where

 Q_R = available flow

 Q_F = observed flow (US GPM)

h_F = drop from measured static to desired baseline pressure

 h_R = drop from measured static to measured residual pressure

Based on flow test results obtained by Lozzi Aqua Check dated September 4, 2019 for the Grenville watermain

$$c = 0.9$$

$$d = 2.5 \text{ in}$$

$$number of ports = 2$$

$$p = 25$$

$$Q_F = 1678 \text{ US GPM}$$

Desired Residual Pressure = 20 psi , minimum per City of Toronto design criteria

Water Demand Design Calculations

Project: 27 Grosvenor & 26 Grenville - Podium

Project No: 18045

Location: Toronto, Ontario
Site Area: 0.3846 ha

Population

· opaiation		
1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

		Commercial			
	1B / 1B+D	1B / 1B+D			
TOTAL UNITS / AREA (m ²)	50	75	64	189	1781.0

		Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential		70	158	199	427
Commercial		-	-	-	20
Total Equivalent Population				447	

City of Toronto Watermain Guidelines

Per Capita Demand

Single Family	310	(L/capita/day)
Multi-Unit	190	(L/capita/day)

Peaking Factors

Land Use	Minimum Hour	Maximum Hour	Maximum Day	
Residential	0.80	2.25	1.50	
Commercial	0.84	1.20	1.10	*Values used for Commercial Land Use
Industrial	0.84	1.90	1.10	
Institutional	0.84	1.90	1.10	
Apartment	0.84	2.50	1.30	*Values used for Residential (Multi-Unit) Land Use

Water Demand based on Equivalent Population

Land Use	Population	Minimum Hour (L/min)	Maximum Hour (L/min)	Maximum Day (L/min)	Fire Flow Required (L/min)	Fire Flow Duration (hr)*	Max Day + Fire Flow (L/min)
Commercial	20	2.2	3.2	2.9	-	-	-
Residential (Multi-Unit)	427	47.3	140.9	73.2	-	-	-
Totals	447	49.5	144.0	76.1	8000	2.00	8,076.1

Project: 27 Grosvenor & 26 Grenville

Project No: 18045

Location:Toronto OntarioSite Area:0.3846

Existing Equivalent Population Calculations

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto $Design\ flow = average\ daily\ dry\ weather\ flow\ x\ peaking\ factor\ + infiltration$

Persons Per Unit and per Land Use

Single Family Dwelling	3.5	ppu
Duplex	2.3	ppu
1BR/1BR+Den	1.4	ppu
2BR/2BR+Den/	2.1	ppu
3BR/3BR+Den	3.1	ppu
Commercial / Retail	1.1	persons/100m ²
Offices	3.3	persons/100m ²

	Reside	Residential Units	
	Single Family Dwelling	Duplex Units	Area (m²)
Existing 2 Storey Office (26 Grenville)	0	-	2362
TOTAL UNITS / AREA (m ²)	3	0	2362

	Single Family Dwelling	TOTAL POPULATION
Residential	0	0
Office	-	77.946
Total Equivalent Population		78

Peak flow Design Parameters

Industrial/Commercial/Office	240	litres/person/day
Infiltration	0.26	litres/second/ha

Harmon Peaking Factor

	Harmon Peak
Total Population	Factor
78	4.27

Average Dry Weather Flow	0.22	L/s
_		
Total Peak Wastewater Flow	0.92	L/s
Infiltration	0.10	L/s
	-	_
Flow	1 02	l /s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (Entire Development)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²

	Residential Units				Commercial
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)
TOTAL UNITS / AREA (m ²)	328	341	101	770	1781

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	460	717	314	1491
Commercial	-	-	-	20
Total Equivalent Population				1511

Peak flow Design Parameters

· · · · · · · · · · · · · · · · · · ·	
Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

	Harmon Peak
Residential Population	Factor
1491	3.68

Residential Flow	15.25	L/s	*based on population
Retail Flow	0.37	L/s	*based on floor area
Groundwater Flows	0.63	L/s	* 10 USGPM pump

Flow	16.25	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (North Tower)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²

	Residential Units				Commercial
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)
TOTAL UNITS / AREA (m ²)	80	101	25	206	0

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	112	213	78	403
Commercial	-	-	-	0
Total Equivalent Population				403

Peak flow Design Parameters

Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

	Harmon Peak
Residential Population	Factor
403	4.02

Residential Flow	4.50	L/s	*based on population
Retail Flow	0.00	L/s	*based on floor area
Groundwater Flows	0.63	L/s	* 10 USGPM pump

Flow	5.13	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (South Tower)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²

		Residential Units				
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)	
TOTAL UNITS / AREA (m ²)	198	165	12	375	0	

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	278	347	38	663
Commercial	-	•	-	0
Total Equivalent Population				663

Peak flow Design Parameters

Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

		•		,,	
					Harmon Peak
Res	identi	al Po	pulat	ion	Factor
		663			3.91

_			
Residential Flow	7.20	L/s	*k
Retail Flow	0.00	L/s	*k
Groundwater Flows	0.00	L/s	

*based	on	population
*based	on	floor area

Flow	7.20	L/s

Project: 27 Grosvenor & 26 Grenville

Project No: 18045 Location: Toronto

Site Area: 0.3846 ha

Proposed Sanitary Flow Calculations (Podium)

As per Design Criteria for Sewers and Watermains - First Edition November 2009 City of Toronto Design flow = average daily dry weather flow x peaking factor + infiltration

Persons Per Unit and per Land Use

1BR/1BR+Den	1.4 ppu
2BR/2BR+Den/	2.1 ppu
3BR/3BR+Den	3.1 ppu
Commercial / Retail	1.1 persons/100m ²
Offices	3.3 persons/100m ²

		Commercial			
	1B / 1B+D	2B / 2B + D	3B / 3B+D	Total Units	Area (m²)
TOTAL UNITS / AREA (m ²)	50	75	64	189	1781

	Population 1BR / 1B + D	Population 2BR / 2BR + D	Population 3BR / 3BR + D	TOTAL POPULATION
Residential	70	158	199	427
Commercial	-	-	-	20
Total Equivalent Population				447

Peak flow Design Parameters

- can non zooigii i aramotoio	
Residential Average flow	240 litres/person/day
Commercial Average flow	180,000 litres/ha/day
Infiltration	0.26 litres/second/ha

Harmon Peaking Factor

	Harmon Peak
Residential Population	Factor
427	4.01

Residential Flow	4.75	L/s	*based on population
Retail Flow	0.37	L/s	*based on floor area
Groundwater Flows	0.00	L/s	

Flow	5.13	L/s